

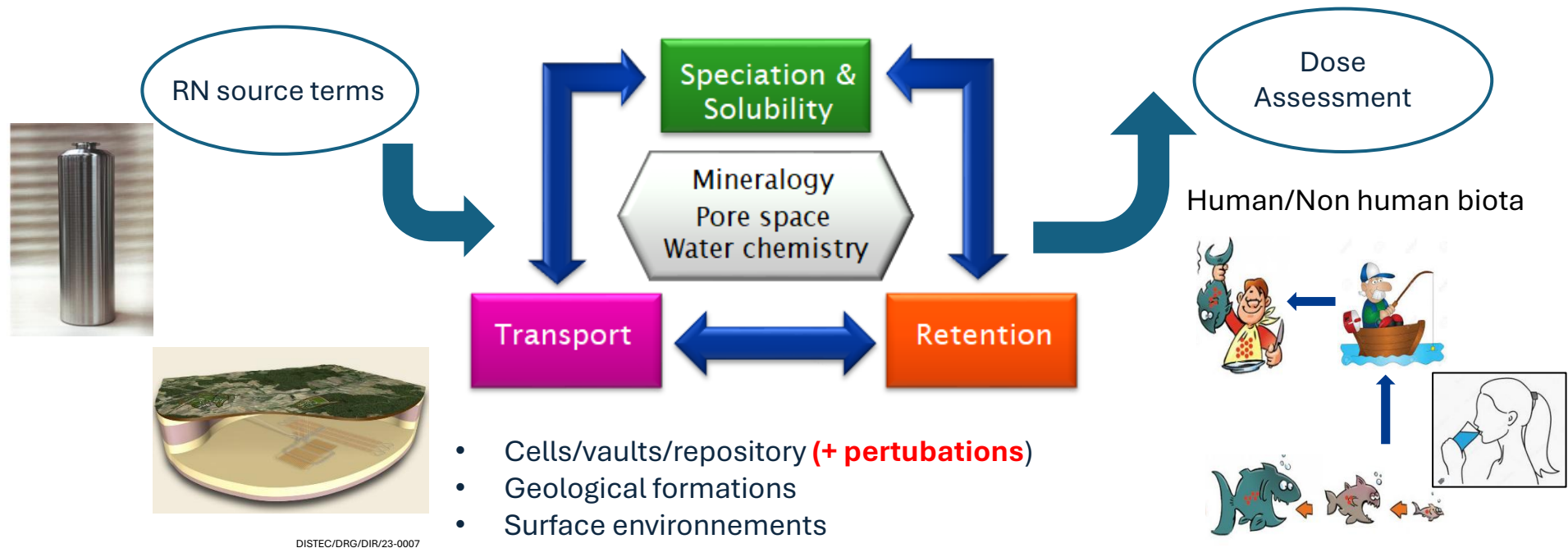
THE USE OF SORPTION DATA IN THE SAFETY CASE - ILLUSTRATION OF THE ANDRA CIGÉO PROJECT

EURAD II annual meeting – September 2027 • P Henocq (Andra) – JC Robinet (Andra)



Co-funded by the European Union under Grant Agreement n° 101166718

Long-term safety assessments aim to calculate the doses resulting from the release of radionuclides from the waste



Accounting for sorption processes must incorporate the requirements of a safety case :

- Robust with respect to process representation
- Manageable for handling various safety scenarios (best-estimate, bounding/envelope, altered, etc.)
- Applicable to all the radionuclides and toxic chemicals concerned



To date the Kd approach remains the most appropriate for carrying out safety calculations

- Simple calculation methods that allow large scales of time and space to be represented
- The independence between radionuclides (as trace elements), which makes it possible to carry out calculations for almost all chemical elements
- Well suited to sensitivity analyses (single- or multi-parameter) allowing to manage the various scenarios

Limitations/implications of using the Kd approach

- Not particularly suitable for disturbed systems with strong geochemical gradients and changes in rock/materials properties over time → needs to adapt (cf. Task 5 of Rampec)
- Collection of data specific to a rock or material
- Selection of **best-estimated values** and a **range of values**
 - There is **no universal method**, and it requires expert judgement and justifications (analogy, statistics, etc.).

How to proceed with sorption data ?

Sorption data are collected (referenced), organized and analyzed to select Kd values to use in the Safety Case

- For **clay-rocks**, each organization has their own “database” (and Kd values selection)
 - Data coming from mainly national programs + additional data coming from international collaborations
 - Natural variability with several locations
 - Effects of perturbations
 - Data on other clays-rocks and pure clays minerals are also collected
- For **cementitious materials** – which are materials used by everyone
 - Data from various national and international projects.
 - For several cement formula
 - For several degradation states
 - Effect of perturbations

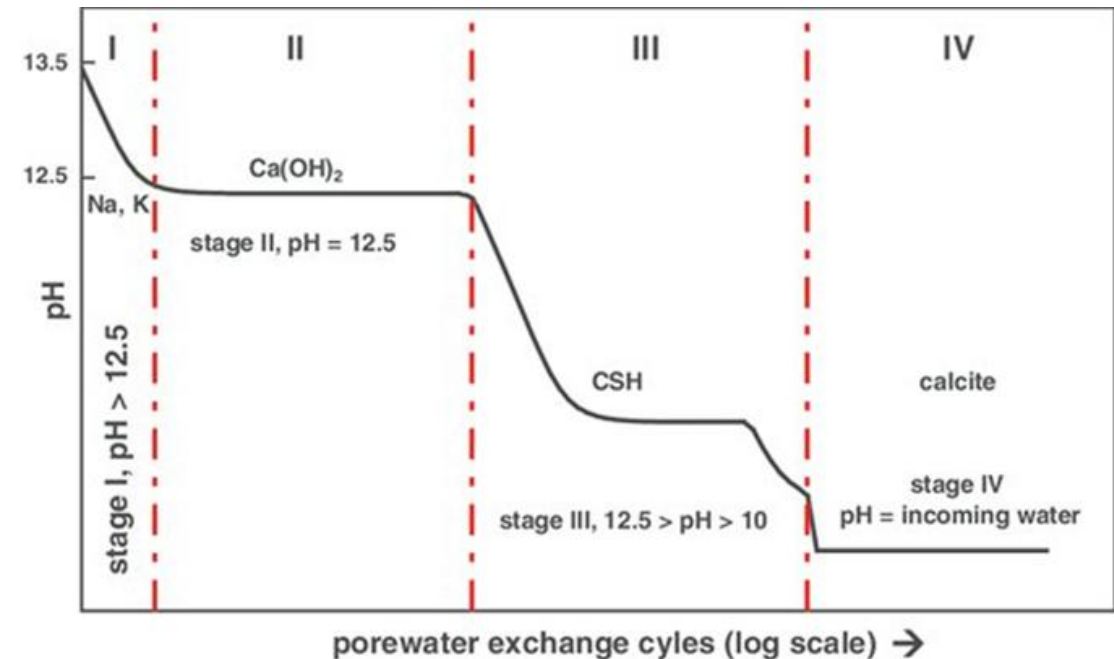
To date, these databases are **not digital databases** containing all the data acquired during sorption tests.

For each chemical element, the robustness of sorption data is analyzed to derive :

- Best-estimate values representative of the repository conditions
- Boundary values including the uncertainties which are related to:
 - Lack of knowledge and data
 - Natural variability for clay-rocks
 - Representativeness of the data toward the repository conditions
 - Concentration effect, competition... but also reversibility, slow kinetic processes

EXAMPLE : SORPTION IN THE CEMENT-BASED MATERIALS

- 4 degradation stages to take into account the chemical evolution with time of the cement-based materials
- 144 radionuclides
- One Kd dataset for each stage
- Kd values applied to all the cement-based Materials :
 - Independently on the formulation (Cement type, W/C)
- Kd determination : Batch experiments
 - Pastes, mortars
 - Individual phases: C-S-H, Ettringite, Afms, Portlandite
- Kd evaluation:
 - Isotherms
 - Empirical models
 - Isotopic models
 - Chemical analogy

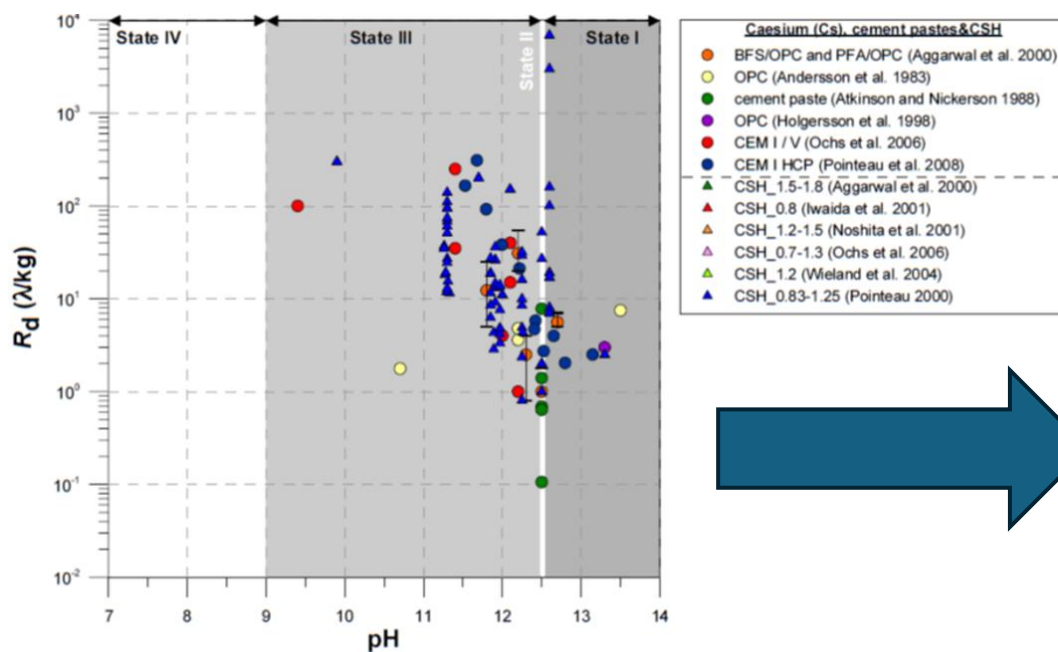


Ochs et al., 2016

A REFERENCE FOR KD VALUES IN CEMENT-BASED MATERIALS

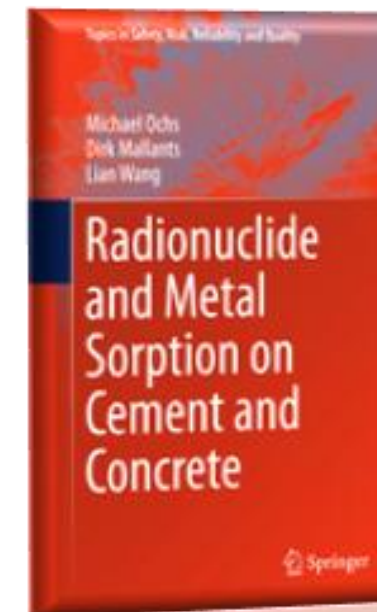
- In the case of cement-based materials, many sorption studies of radionuclides have been carried out in Europe and in many countries
- In 2009 and 2011, an european review of Kd values for the main radionuclides (25) in cement-based materials has been released by Ondraf/NIRAS (Wang et al., 2009 & 2011) and published by Ochs et al. (2016)

• Approach:



pH state	Best estimate (l/kg)	Upper limit (l/kg)	Lower limit (l/kg)
State I	i.d.	10^1	1×10^{-1}
State II	2×10^0	5×10^1	1×10^{-1}
State III	2×10^1	3×10^2	1×10^0
State IV	i.d.	i.d.	i.d.

Event



Ochs et al., 2016

eurad²

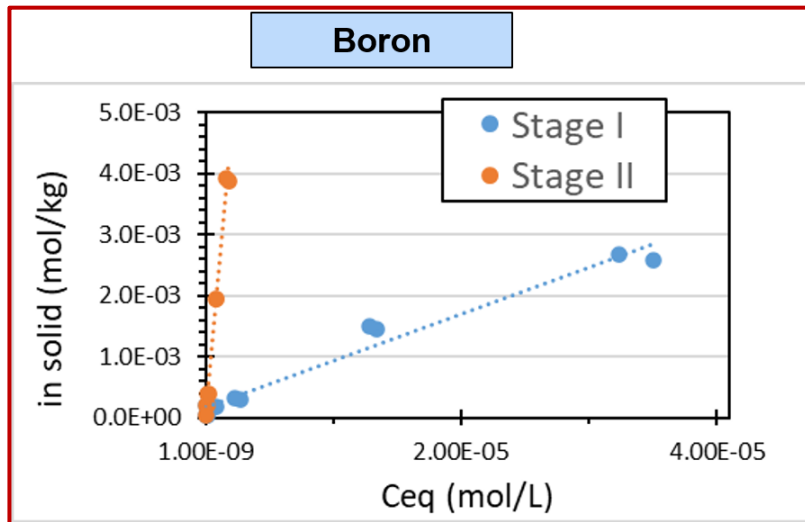
EXAMPLE : SORPTION IN THE CEMENT-BASED MATERIALS

- Database of Kd values (extract)
- Best-estimate & Range of values
- Stage I

Element	Kd (m ³ .kg ⁻¹)	Range of values	Element	Kd (m ³ .kg ⁻¹)	Range of values
HTO	0	-	Sm	10	0,1 - 5 000
Be	5	1 - 50	Gd		
B	1 × 10 ⁻¹	5 × 10 ⁻³ - 2,5 × 10 ⁻¹	Dy		
C(IV)	2	0,5 - 3	Ho		
C(-IV)	-	-	Lu		
Al	-	-	Hf	-	-
Cl	2 × 10 ⁻²	5 × 10 ⁻³ - 5 × 10 ⁻²	Re	1 × 10 ⁻³	-
K	-	-	Hg	-	-
Ca	7 × 10 ⁻³	2 × 10 ⁻³ - 2,3 × 10 ⁻²	Pb	0,3	0,1 - 1
Cr	10	0,1 - 5000	Sr	0,1	0,03 - 0,3
Mn	-	-	Ra	0,3	0,1 - 1
Ni	6,5 × 10 ⁻²	3 × 10 ⁻² - 7,3 × 10 ⁻¹	Th	30	1 - 1 000

EXAMPLE : SORPTION IN THE CEMENT-BASED MATERIALS

- Database of K_d values (extract)
- Stage I
- Boron (B) - Isotherm



Element	K _d (m ³ .kg ⁻¹)	Range of values	Element	K _d (m ³ .kg ⁻¹)	Range of values
HTO	0	-	Sm	10	0,1 - 5 000
Be	5	1 - 50	Gd		
B	1 × 10 ⁻¹	5 × 10 ⁻³ - 2,5 × 10 ⁻¹	Dy		
C(IV)	2	0,5 - 3	Ho		
C(-IV)	-	-	Lu	-	-
Al	-	-	Hf		
Cl	2 × 10 ⁻²	5 × 10 ⁻³ - 5 × 10 ⁻²	Re	1 × 10 ⁻³	-
K	-	-	Hg	-	-
Ca	7 × 10 ⁻³	2 × 10 ⁻³ - 2,3 × 10 ⁻²	Pb	0,3	0,1 - 1
Cr	10	0,1 - 5000	Sr	0,1	0,03 - 0,3
Mn	-	-	Ra	0,3	0,1 - 1
Ni	6,5 × 10 ⁻²	3 × 10 ⁻² - 7,3 × 10 ⁻¹	Th	30	1 - 1 000

EXAMPLE : SORPTION IN THE CEMENT-BASED MATERIALS

- Database of Kd values (extract)
- Stage I
- Nickel (Ni) – Isotopic model

Conditions	R_{d,M^*} [m ³ kg ⁻¹]	$R_{d,M}$ [m ³ kg ⁻¹]	α
No Ni addition	0.15 ± 0.02	4.6 ± 2.3	$(3.3 \pm 1.7) \times 10^{-2}$
$[\text{Ni}]_{\text{add}} = 10^{-6} \text{ M}$			
7 days equilibration	0.22 ± 0.02	4.9 ± 1.0	$(4.5 \pm 1.0) \times 10^{-2}$
30 days equilibration	0.20 ± 0.02	6.9 ± 1.4	$(2.9 \pm 0.6) \times 10^{-2}$
$[\text{Ni}]_{\text{add}} = 10^{-4} \text{ M}$			
7 days equilibration	1.1 ± 0.1	38.6 ± 7.5	$(2.8 \pm 0.6) \times 10^{-2}$
30 days equilibration	1.2 ± 0.1	26.8 ± 5.4	$(4.5 \pm 1.0) \times 10^{-2}$

Partition coefficient:

$$\alpha = \frac{(n_{s,M^*}/n_{s,M})}{(n_{l,M^*}/n_{l,M})} = \frac{R_{d,M^*}}{R_{d,M}}$$

Wieland et al. (2006)

Element	Kd (m ³ .kg ⁻¹)	Range of values	Element	Kd (m ³ .kg ⁻¹)	Range of values
HTO	0	-	Sm	10	0,1 - 5 000
Be	5	1 - 50	Gd		
B	1×10^{-1}	$5 \times 10^{-3} - 2,5 \times 10^{-1}$	Dy		
C(IV)	2	0,5 - 3	Ho		
C(-IV)	-	-	Lu	-	-
Al	-	-	Hf		
Cl	2×10^{-2}	$5 \times 10^{-3} - 5 \times 10^{-2}$	Re		
K	-	-	Hg	-	-
Ca	7×10^{-3}	$2 \times 10^{-3} - 2,3 \times 10^{-2}$	Pb	0,3	0,1 - 1
Cr	10	0,1 - 5000	Sr	0,1	0,03 - 0,3
Mn	-	-	Ra	0,3	0,1 - 1
Ni	$6,5 \times 10^{-2}$	$3 \times 10^{-2} - 7,3 \times 10^{-1}$	Th	30	1 - 1 000

EXAMPLE : SORPTION IN THE CEMENT-BASED MATERIALS

- Database of K_d values (extract)
- Stage I
- Lanthanides – Am as analogue

Chemical analogy with Am

Element	K _d (m ³ .kg ⁻¹)	Range of values	Element	K _d (m ³ .kg ⁻¹)	Range of values
HTO	0	-	Sm	10	0,1 - 5 000
Be	5	1 - 50	Gd		
B	1 × 10 ⁻¹	5 × 10 ⁻³ - 2,5 × 10 ⁻¹	Dy		
C(IV)	2	0,5 - 3	Ho		
C(-IV)	-	-	Lu		
Al	-	-	Hf	-	-
Cl	2 × 10 ⁻²	5 × 10 ⁻³ - 5 × 10 ⁻²	Re	1 × 10 ⁻³	-
K	-	-	Hg	-	-
Ca	7 × 10 ⁻³	2 × 10 ⁻³ - 2,3 × 10 ⁻²	Pb	0,3	0,1 - 1
Cr	10	0,1 - 5000	Sr	0,1	0,03 - 0,3
Mn	-	-	Ra	0,3	0,1 - 1
Ni	6,5 × 10 ⁻²	3 × 10 ⁻² - 7,3 × 10 ⁻¹	Th	30	1 - 1 000

CONCLUSION

- **A Kd model is widely used to support the safety assessments**
 - Suitable for many cases
 - Easily manageable in terms of modelling
 - Simplifications inducing uncertainties → several sorption mechanisms do not verified the Kd conditions (incorporation, isotopic exchange,...)
- **A Kd value is associated to**
 - One system : a given solution in equilibrium with the solid (clay- or cement-based materials)
 - → if the system evolves, Kd should modify (need to have the corresponding experimental data)
- **The safety case need to collect Kd data**
 - Numerical database with all experimental conditions is not required
 - But justifications of how the Kd is selected are needed
 - For cement based materials, international initiatives could be generalized to create (numerical) databases
- **Further comparisons between Kd and geochemical models are required for disturbed systems**
 - Aim of WP RAMPEC : TASKs 4&5